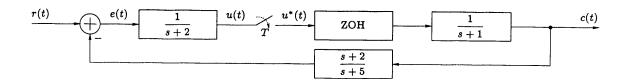
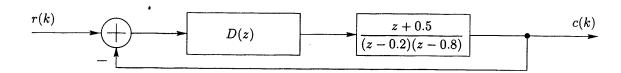
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1. Consider the following system with a sampling period T=0.1 second. Obtain an expression for the transfer function C(z)/R(z). (50pts)



2. Consider the following feedback control system with a sampling period T = 0.1 second.



(a) Assume a PI controller in the form

$$D(z) = K_1 + \frac{K_2}{z-1}.$$

Choose K_2 (in terms of K_1), such that the slowest open-loop pole is canceled, and determine the range of stability for all K_1 with this choice of K_2 . (20pts)

(b) Design a first-order compensator such that

$$D(z) = K \frac{z - z_1}{z - p_1},$$

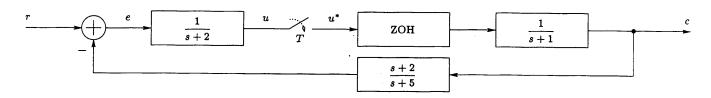
where K, z_1 , and p_1 are the gain, the zero, and the pole of the compensator, respectively, such that the following conditions are satisfied.

- i. The maximum percent overshoot is between 1% and 3% for a unit step input.
- ii. The 2% settling time is less than 0.4 second.

(30pts)

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1. Consider the following system with a sampling period T = 0.1 second. Obtain an expression for the transfer function C(z)/R(z).



Solution: Assuming that there are pseudo samplers at the input and the output, we write the relationships among pseudo sampled signals.

$$C^*(s) = \frac{1}{s+1}G_{\text{ZOH}}(s)U^*(s),$$

where $(\cdot)^*$ represents a pseudo sampled signal, and $G_{\text{ZOH}}(s)$ is the transfer function of the zero-order hold (ZOH). So,

$$C(z) = \frac{z-1}{z} \mathcal{Z} \left[\mathcal{L}^{-1} \left[\frac{1}{s(s+1)} \right] \right] U(z).$$

Also

$$U^*(s) = \frac{1}{s+2} \left(R^*(s) - \left(\frac{s+2}{s+5} \right) \left(\frac{1}{s+1} \right) G_{\text{ZOH}}(s) U^*(s) \right),$$

or

$$\left(1 + \frac{1}{(s+1)(s+5)}G_{\text{ZOH}}(s)\right)U^*(s) = \frac{1}{s+2}R^*(s),$$

and

$$\left(\mathcal{Z}\left[\mathcal{L}^{-1}\left[1\right]\right] + \frac{z-1}{z}\mathcal{Z}\left[\mathcal{L}^{-1}\left[\frac{1}{s(s+1)(s+5)}\right]\right]\right)U(z) = \mathcal{Z}\left[\mathcal{L}^{-1}\left[\frac{1}{s+2}\right]\right]R(z).$$

Solving for U(z) from the above equation and substituting into the expression for C(z), we get

$$\frac{C(z)}{R(z)} = \frac{\frac{z-1}{z} \mathcal{Z} \left[\mathcal{L}^{-1} \left[\frac{1}{s(s+1)} \right] \right] \mathcal{Z} \left[\mathcal{L}^{-1} \left[\frac{1}{s+2} \right] \right]}{1 + \frac{z-1}{z} \mathcal{Z} \left[\mathcal{L}^{-1} \left[\frac{1}{s(s+1)(s+5)} \right] \right]}.$$

Next, we need to determine all the z transforms of the inverse Laplace transforms. So consider

$$\frac{z-1}{z} \mathcal{Z} \left[\mathcal{L}^{-1} \left[\frac{1}{s(s+1)} \right] \right] = \frac{z-1}{z} \mathcal{Z} \left[\mathcal{L}^{-1} \left[\frac{1}{s} - \frac{1}{s+1} \right] \right]$$

$$= \frac{z-1}{z} \left[\frac{z}{z-1} - \frac{z}{z-e^{-T}} \right]$$

$$= 1 - \frac{z-1}{z-e^{-T}} = \frac{1-e^{-T}}{z-e^{-T}} \approx \frac{0.0952}{z-0.9048},$$

$$\mathcal{Z}\left[\mathcal{L}^{-1}\left[\frac{1}{s+2}\right]\right] = \frac{z}{z - e^{-2T}} \approx \frac{z}{z - 0.8187},$$

and

$$\begin{split} \frac{z-1}{z} \mathcal{Z} \left[\mathcal{L}^{-1} \left[\frac{1}{s(s+1)(s+5)} \right] \right] &= \frac{z-1}{z} \mathcal{Z} \left[\mathcal{L}^{-1} \left[\frac{1/5}{s} - \frac{1/4}{s+1} + \frac{1/20}{s+5} \right] \right] \\ &= \frac{z-1}{z} \left[(1/5) \frac{z}{z-1} - (1/4) \frac{z}{z-e^{-T}} + (1/20) \frac{z}{z-e^{-5T}} \right] \\ &= \frac{1}{5} - \frac{z-1}{4(z-e^{-T})} + \frac{z-1}{20(z-e^{-5T})} \\ &= \frac{1}{5} - \frac{(z-1)(4z-(5e^{-5T}-e^{-T}))}{20(z-e^{-T})(z-e^{-5T})} \\ &\approx \frac{1}{5} - \frac{(z-1)(4z-2.1278)}{20(z-0.9048)(z-0.6065)}. \end{split}$$

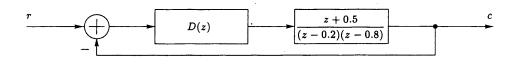
Substituting all the expressions into the C(z)/R(z) expression gives

$$\frac{C(z)}{R(z)} = \frac{\left(\frac{1 - e^{-T}}{z - e^{-T}}\right) \left(\frac{z}{z - e^{-2T}}\right)}{1 + \left(\frac{1}{5} - \frac{(z - 1)(4z - (5e^{-5T} - e^{-T}))}{20(z - e^{-T})(z - e^{-5T})}\right)}.$$

After rearranging some of the expressions above, we have

$$\begin{split} \frac{C(z)}{R(z)} &= \frac{20(1-e^{-T})z(z-e^{-5T})}{\left(24(z-e^{-T})(z-e^{-5T})-(z-1)(4z-(5e^{-5T}-e^{-T}))\right)\left(z-e^{-2T}\right)} \\ &\approx \frac{1.9033z(z-0.6065)}{\left(24(z-0.9048)(z-0.6065)-(z-1)(4z-2.1278)\right)(z-0.8187)}. \end{split}$$

2. Consider the following feedback control system with a sampling period T = 0.1 second.



(a) Assume a PI controller in the form

$$D(z) = K_1 + \frac{K_2}{z - 1}.$$

Choose K_2 (in terms of K_1), such that the slowest open-loop pole is canceled, and determine the range of stability for all K_1 with this choice of K_2 .

Solution: Rewriting the controller, we have

$$D(z) = K_1 + \frac{K_2}{z - 1} = \frac{K_1(z - 1) + K_2}{z - 1} = K_1 \frac{z - (1 - K_2/K_1)}{z - 1}.$$

Since the slowest pole is at 0.8, we choose the zero of the controller, such that

$$1 - K_2/K_1 = 0.8$$
,

or

$$K_2 = 0.2K_1$$
.

For this choice, the controller becomes

$$D(z) = K_1 \frac{z - 0.8}{z - 1}.$$

The poles of the closed-loop system can be determined from the solution of the characteristic equation 1 + D(z)G(z) = 0, where G(z) is the plant transfer function, so

$$(z - 0.2)(z - 1) + K_1(z + 0.5) = 0,$$

$$z^2 + (K_1 - 1.2)z + (0.5K_1 + 0.2) = 0.$$

To determine the range of stability for all K_1 , we can use Jury's stability test criteria. Since the characteristic polynomial $q(z) = z^2 + (K_1 - 1.2)z + (0.5K_1 + 0.2)$, the order of the system n = 2. The two boundary conditions are

$$q(1) > 0,$$

 $(1)^2 + (K_1 - 1.2)(1) + (0.5K_1 + 0.2) > 0,$
 $K_1 > 0,$ (2.1)

and

$$(-1)^{n}q(-1) > 0,$$

$$(-1)^{2}((-1)^{2} + (K_{1} - 1.2)(-1) + (0.5K_{1} + 0.2)) > 0,$$

$$K_{1} < 4.8.$$
(2.2)

The pole-product condition is

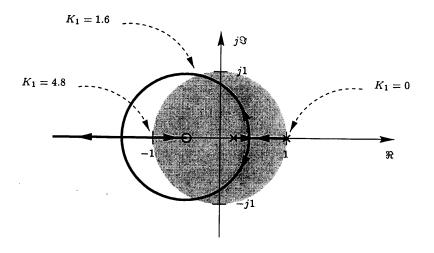
$$|a_0| < a_n,$$

 $|0.5K_1 + 0.2| < 1,$
 $-1 < 0.5K_1 + 0.2 < 1,$
 $-2.4 < K_1 < 1.6.$ (2.3)

The rest of the conditions are to be obtained from the Jury's table. However, since we have a second-order system, the table will not give any additional conditions. From the intersection of the regions described by Inequalities 2.1–2.3, we conclude that the system will be stable, when

$$0 < K_1 < 1.6$$
.

The regions described by İnequalities 2.1–2.3 can also be observed from the root-locus diagram of the system for $K_1 \geq 0$.



(b) Design a first-order compensator such that

$$D(z) = K \frac{z - z_1}{z - p_1},$$

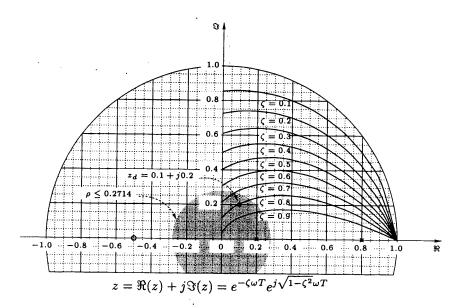
where K, z_1 , and p_1 are the gain, the zero, and the pole of the compensator, respectively, such that the following conditions are satisfied.

- i. The maximum percent overshoot is between 1% and 3% for a unit step input.
- ii. The 2% settling time is less than 0.4 second.

Solution: We determine the restrictions on the location of the desired pole locations from the performance specifications.

Given Requirements	General System Restrictions	Specific System Restrictions
Maximum percent overshoot for a unit step input	$0.01 < M_p < 0.03.$	From the α - M_p curves, $\zeta = 0.8$ provides the broadest range of α values, where $-80^\circ < \alpha < 5^\circ$.
Settling time for a unit step input	$\rho \le (0.02)^{1/(k_{2\%s}-1)}.$	For $t_{2\%s} = k_{2\%s}T \le 0.4 \mathrm{s}$, and $k_{2\%s} \le 0.4/0.1 = 4$, when $T = 0.1 \mathrm{s}$; $\rho \le (0.02)^{1/(4-1)} = 0.2714.$

When we mark these restrictions on the z-plane, we determine that a possible set of desired pole locations is at $z_d \approx 0.1 \pm j0.2$.



The deficiency angle, ϕ , needed at the desired location to ensure that one of the root-locus branches goes through the location, can be determined from the angular condition.

$$\phi + \angle(z_d - (-0.5)) - \angle(z_d - (0.2)) - \angle(z_d - (0.8)) = (2k+1)\pi,$$

for an integer k. For $z_d = 0.1 + j0.2$,

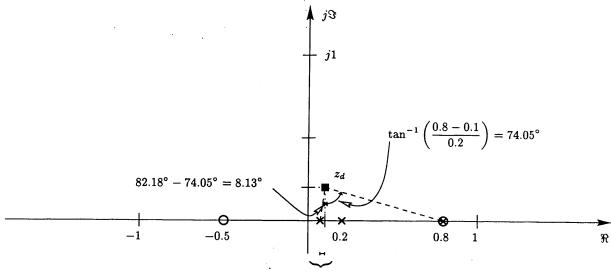
$$\phi + \tan^{-1}\left(\frac{(0.2) - (0)}{(0.1) - (-0.5)}\right) - \tan^{-1}\left(\frac{(0.2) - (0)}{(0.1) - (0.2)}\right) - \tan^{-1}\left(\frac{(0.2) - (0)}{(0.1) - (0.8)}\right)$$

$$= 180^{\circ} + k360^{\circ},$$

$$\phi + 18.43^{\circ} - 116.57^{\circ} - 164.05^{\circ} = 180^{\circ} + k360^{\circ},$$

or $\phi = 82.18^{\circ}$.

In order to preserve the system order so that transient specifications stay accurate, we need to cancel a pole or zero and place another one in such a way that the pole-zero combination provides the necessary deficiency angle at z_d . The best choice for cancelation is the pole at 0.8, since it is the slowest.



 $0.2 \tan(8.13^{\circ}) = 0.0286 \Longrightarrow \text{pole} = 0.1 - 0.0286 = 0.0714$

From the above analysis,

$$D(z) = K \frac{z - 0.8}{z - 0.0714}.$$

And the magnitude K is obtained from the magnitude condition at z_d .

$$|D(z)G(z)|_{z=z_d}=1,$$

$$\left| K \frac{z + 0.5}{(z - 0.0714)(z - 0.2)} \right|_{z = 0.1 + j0.2} = 1,$$

or K=0.0714. Therefore, one possible compensator is

$$D(z) = 0.0714 \frac{z - 0.8}{z - 0.0714}.$$